

Overcoming the Challenges to Complete the Central Cordillera Crossing

La Linea Tunnel



November, 2023

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Calarcá - Cajamarca La Linea tunnel





Expected reduction
of accidents

95%



Average speed
increase

**15 km/h to
60 km/h**



The transit between
Calarcá and Cajamarca
will take

**30-50
min**

for light or heavy vehicles.
Previously, this journey
could take up to 3 hours



Reduction of

850
hours per year

of road closures



Travel savings of

12 km


due to reduction of
road length

Budget = Approx.. USD \$ 850 million.

La Línea Tunnel = 8.6 km – Longest road Tunnel in operation in LATAM.

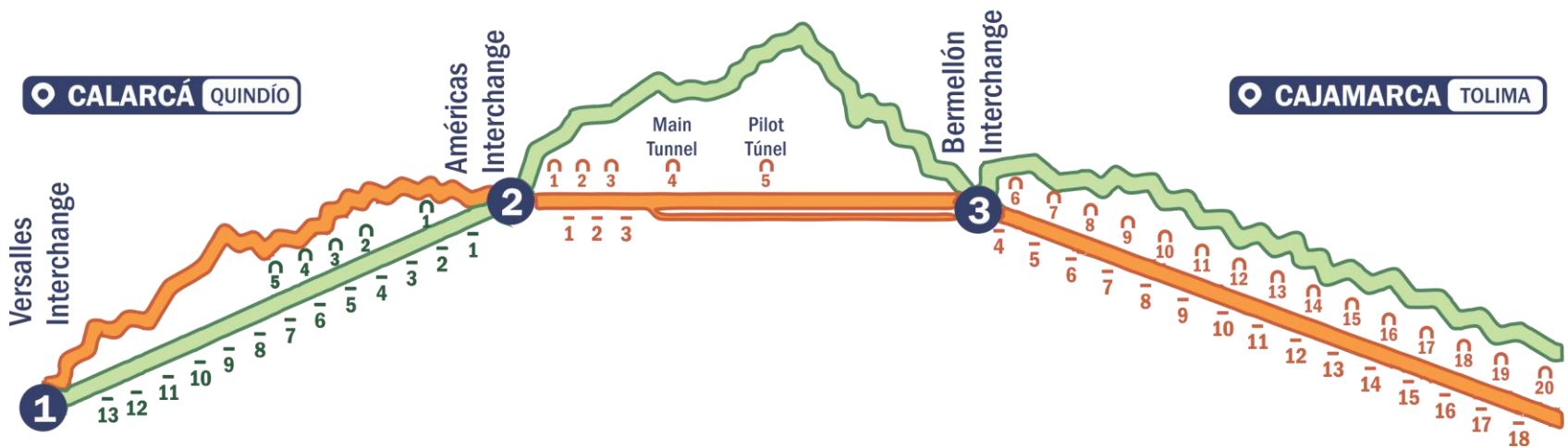
CONVENTIONS

- Works in the direction of Cajamarca - Calarcá
- Works in the direction of Calarcá - Cajamarca
- Tunnels – Bridges ● Interchange



60 WORKS

- 30 km New double traffic lanes
- 40 km Of improved road
- 25 tunnels (22 km)
- 31 bridges (5 km)
- 3 Interchanges



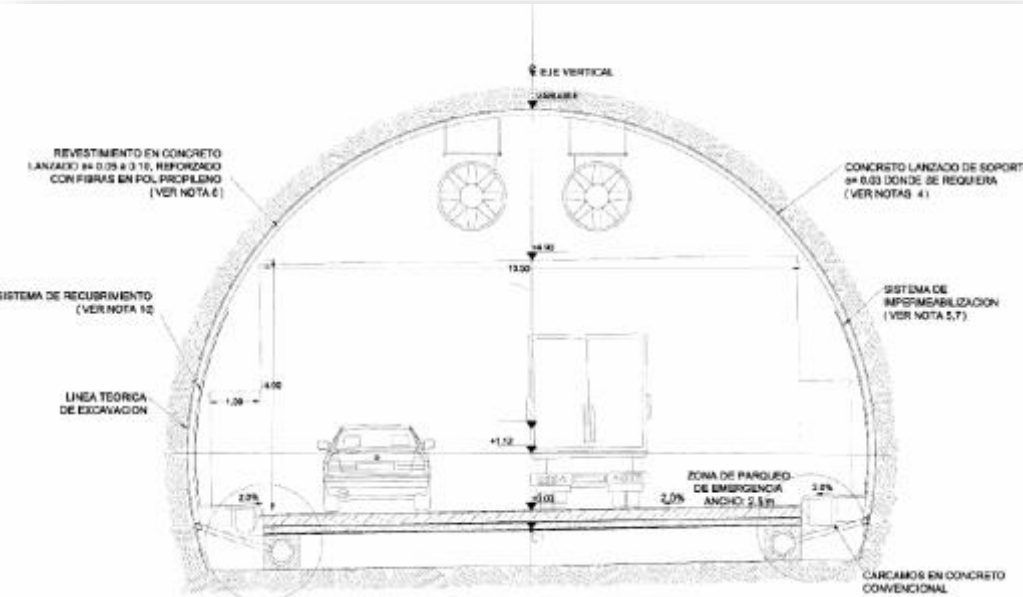
Beginning



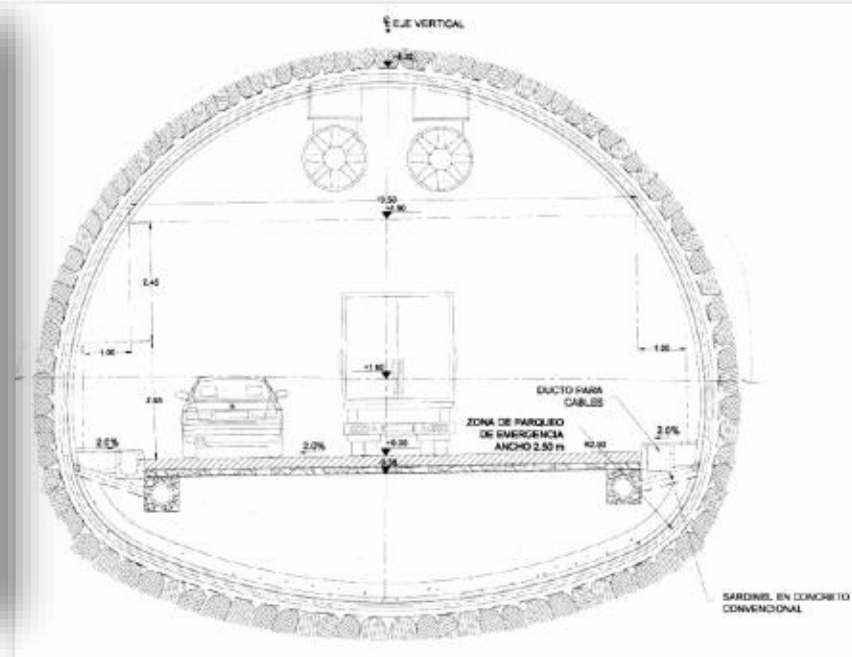
L=640M



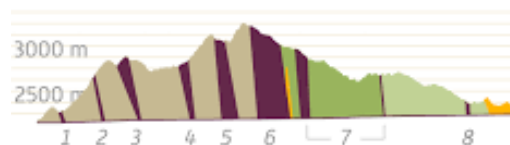
Flat Invert Section



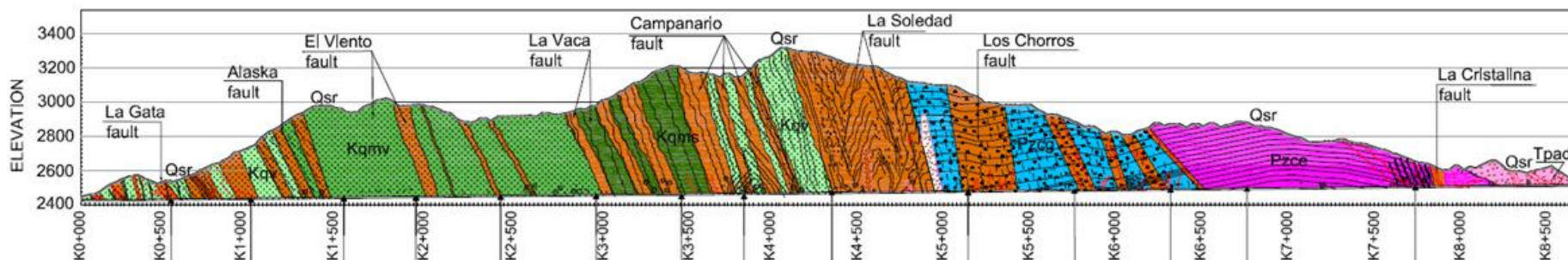
Curved Invert Section










- Length= 8651,57 m
- Semi-circular section (variable radii depending on ground type)
- 2 traffic lanes $w=3,65$ m.
- Safety zone $w= 0,35$ m, each lane.
- Safety parking zones with extra width of 2.5m
- 1m Sidewalks
- 4.9 m minimum clearance on on each side.

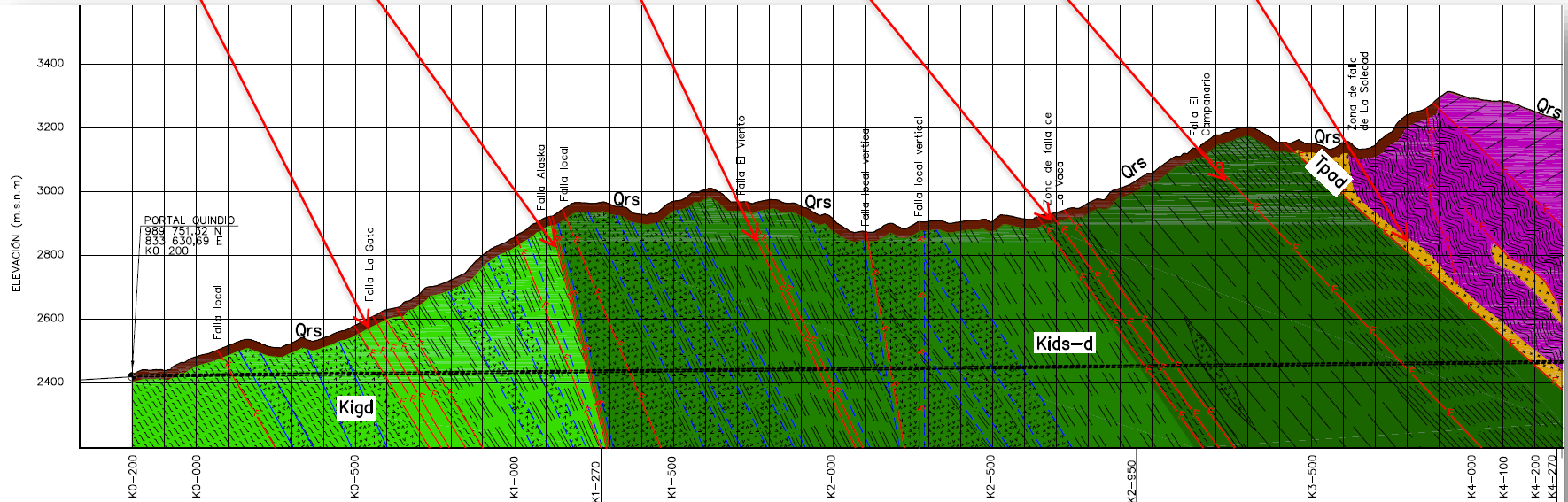


- 1- Zona de Influencia - Falla La Gata
- 2- Zona de Influencia - Falla Alaska
- 3- Falla El Viento
- 4- Falla La Vaca
- 5- Falla Campanario
- 6- Falla La Soledad
- 7- Zona de Influencia Falla Los Chorros
- 8- Falla La Cristalina



- | | | | |
|---|---|---|--|
| <p> Tpad</p> <p> Kqv</p> <p> Kqmv</p> <p></p> | <p>Volcanic porphyry and andesites rocks, aphanitic texture and high hardness.</p> <p>Sedimentary volcanic unit of green and gray diabases and metadiabases, partially foliated.</p> <p>Metamorphic unit of Cajamarca Grande complex chloritic quartz green schists, metadiabases, basalts.</p> <p>Fault zone</p> | <p> Kqms</p> <p> Pzcg</p> <p> Pzce</p> | <p>Sedimentary volcanic unit of metadiabases (phyllites), meta shales, metasandstones, of carbonaceous quartz composition.</p> <p>Blue-green and grayish gabbros, hard with gneissic texture, with some interspersed hard gray schists.</p> <p>Cajamarca complex of green schists and sericite quartz of tin hardness, interspersed with graphite black schists.</p> |
|---|---|---|--|

F. La Gata F. Alaska F. El viento F. La vaca F. Campanario F. La Soledad



UTOLÓGIA	Qrs	Kigd - Complejo Quebradagrande. Diabasas y metadiabasas					Kids-d - Complejo Quebradagrande. Lulitas, pizarras, metareniscas y diabasas.									
GRADO ALTERACIONES O FRACTURACIÓN	Suelo residual y roca alterada.	Roca muy fracturada a moderadamente fracturada.	Roca meteorizada y fracturada.	Roca alterada y fracturada.	Roca fracturada a moderadamente fracturada o poco meteorizada.	Roca alterada y fracturada.	Roca fresca a poco meteorizada poco fracturada.	Roca muy fracturada.	Roca fresca a poco meteorizada de poco a medianamente fracturada.	Roca muy fracturada o moderadamente fracturada.	Roca muy fracturada.	Roca medianamente fracturada a poco fracturada.	Roca fracturada a medianamente fracturada.	Roca fracturada meteorizada.	Roca medianamente fracturada a poco fracturada.	Roca muy fracturada o medianamente fracturada.

CONVENCIONES

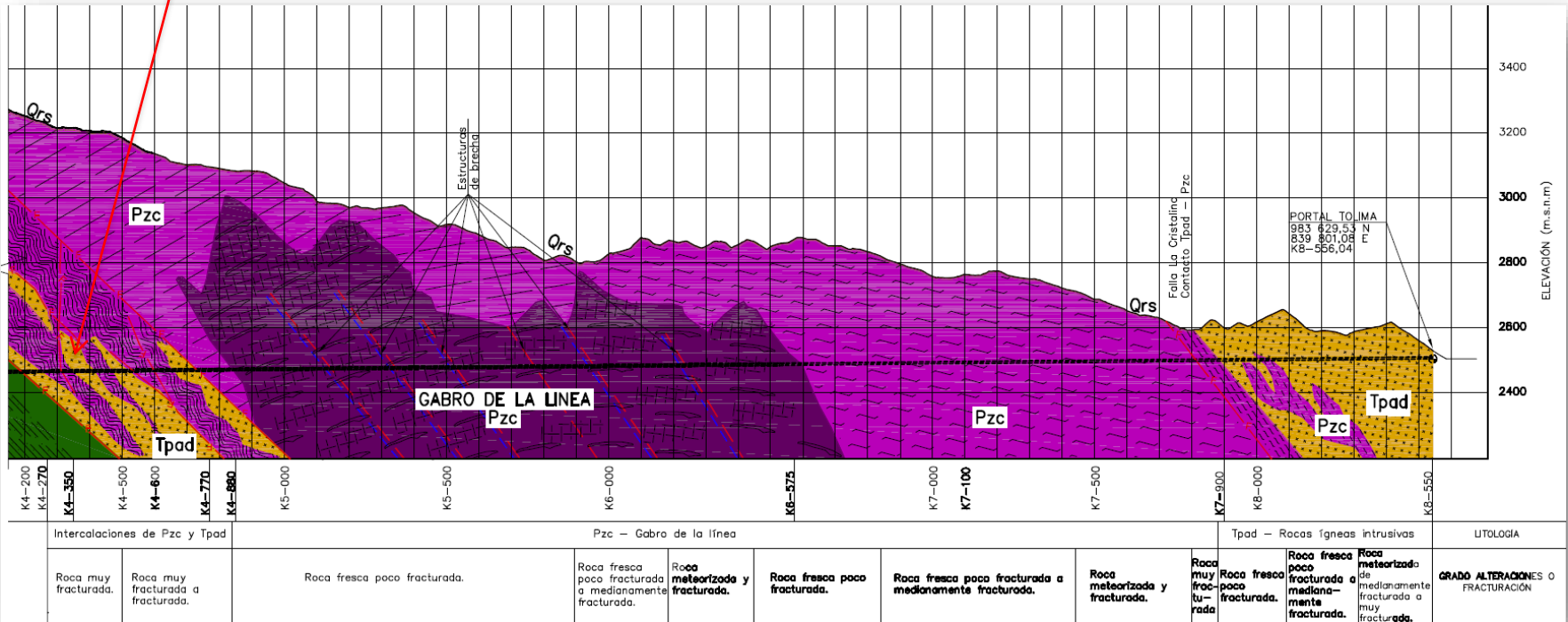
UNIDADES LITOLÓGICAS

- Kigd** Complejo Quebradagrande. Cretáceo - Volcánico tectonizado. Diabasas y metadiabasas.
- Kids-d** Complejo Quebradagrande. Cretáceo - Sedimentario volcánico. Lulitas, pizarras, metareniscas y diabasas.
- Tpad** Rocas ígneas intrusivas porfíricas andesico dacitas.
- Pzc** Gabro de la Línea.
- Qrs** Suelo residual.

Metasedimentary – volcanic rocks

Ingetec (2008)

F. La Soledad



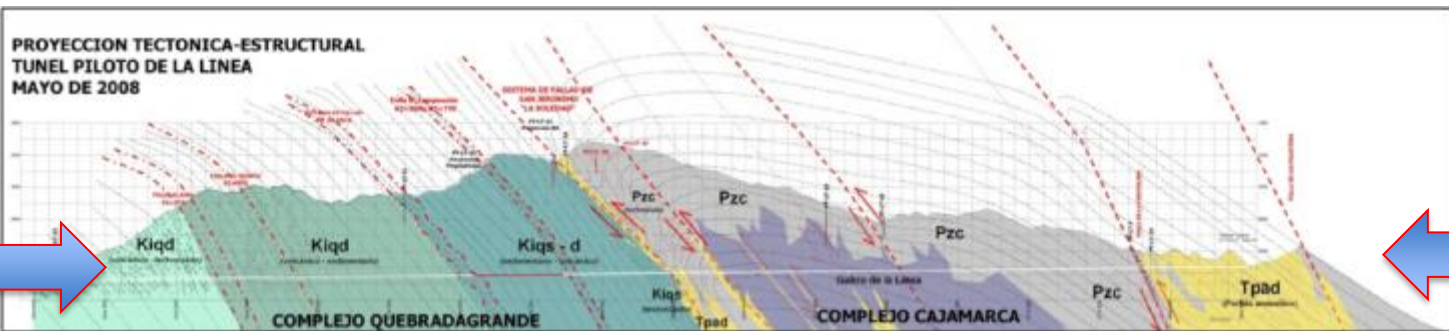
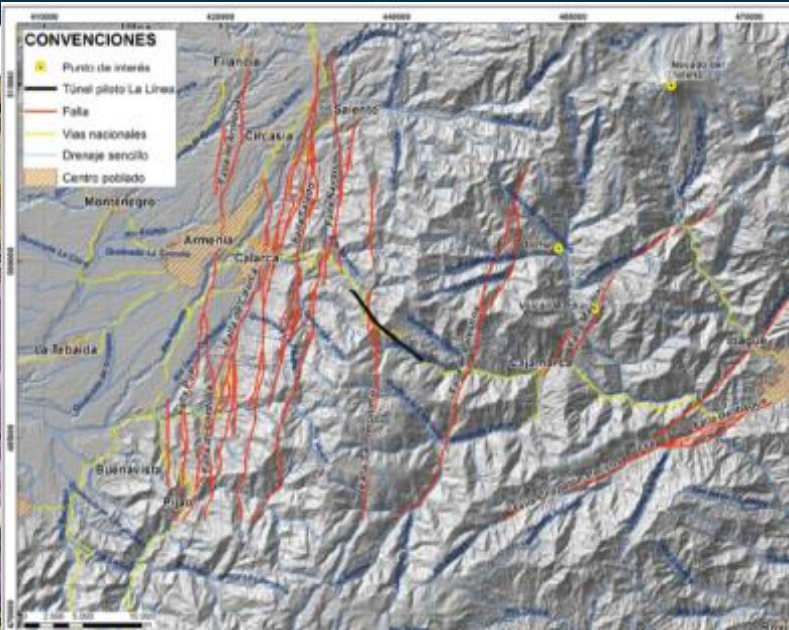
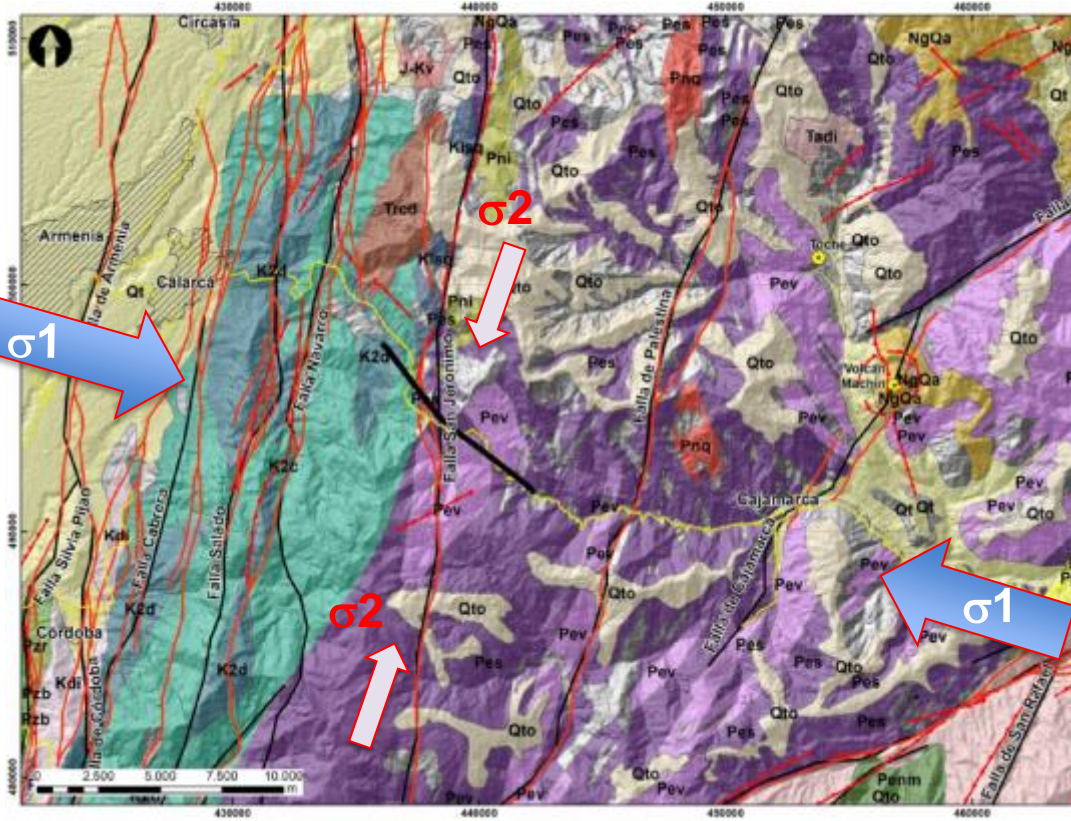
Igneous rocks

Ingetec (2008)

CONVENCIONES

UNIDADES LITOLÓGICAS

- Klgd** Complejo Quebradagrande. Cretáceo - Volcánico tectonizado. Diabasas y metadiabasas.
- Klds-d** Complejo Quebradagrande. Cretáceo - Sedimentario volcánico. Lulitas, pizarras, metareniscas y diabasas.
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- Pzc** Gabro de la Línea.
- Qrs** Suelo residual.



$K = \sigma_h / \sigma_v$

1

Turnkey type of contract. **Lump sum. All geological risk transferred to contractor.**

Contract Value in 2008 approx. USD 315m (\$629.052 million Col. Pesos. Final value of \$975.511 million. Increase of \$346.459 million. (55% increase of initial budget)

2

Contract initial period 70 months. Should have been completed by 2015. Four extensions, adding to 39 additional months. (55% extra time).

3

Significant quality problems. Supposedly only 12% of scope was pending.

4

The technical solutions to stabilize the most challenging fault sections were ineffective.

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1

It is the Owner who will benefit from the completed project. Thus, the ground belongs to the project Owner.

2

The Owner has the responsibility to pay reasonable costs required to handle ground conditions.

3

Risk should be allocated to the party that can best control it.

4

Transferring the geological or geotechnical risk completely to the contractor gives the owner a false sense of security.

5

Balanced and equitable allocation of ground related risks leads to lower cost of the works and more competitive bids.

6

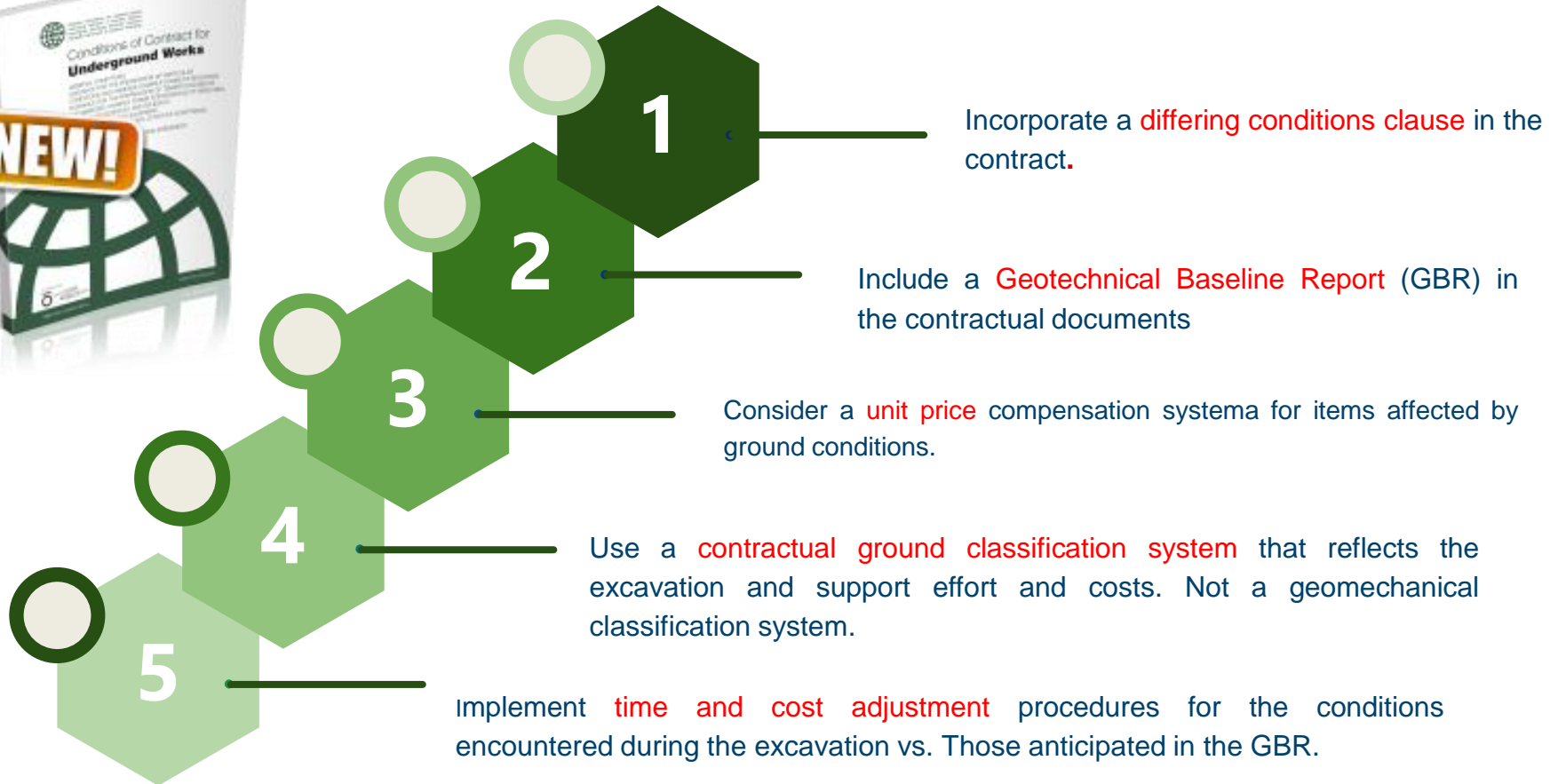
A changed conditions clause should be included in underground construction contracts. Disclaimers and exculpatory language should be eliminated.

7

All available data and interpretations should be disclosed to bidders.

8

Alternative dispute mechanisms implemented





Risk should be allocated to the party better positioned to assume it:

Ground related risk.

Varying site conditions from those anticipated in the contract documents=> Assigned to the **Owner.**

Performance related risk (unit rates) for the anticipated conditions assigned to the Contractor.

1

Unit Price based contract

2

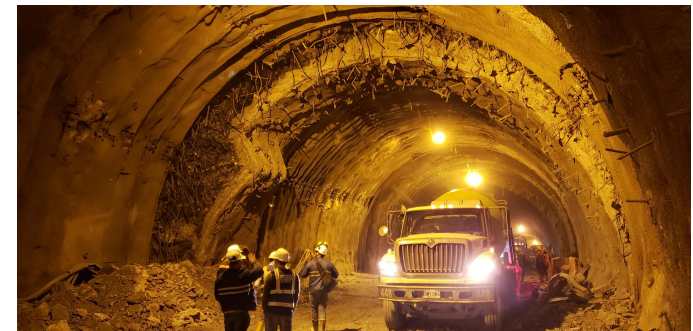
First activity included a diagnosis of the Works after the termination of the UTSC contract

3

Included designs to finalize the project

4

Effective solutions implemented to stabilize the fault zones and finish the Works.



- 1 Main tunnel in **marginal safety condition** in fault zones. Severe convergences. Continued deformations.
- 2 **Much larger loads on the concrete lining than those considered in the design.**
- 3 No provision for reactivation of squeezing due to roc **rock creep**.
- 4 **Deficient and incomplete** documentation of the works.
- 5 **Incomplete support**. Steel arches without support. Rigid arches and incomplete round inverts in zones of squeezing.
- 6 **Cracking and fissures in the shotcrete of the pilot** due to stress distribution. Also in zones where concrete lining had already been installed.
- 7 **Drainage and impermeable geomembrane problems** @ main and short tunnels. Exposed geomembranes.
- 8 Deficient geologic registers. **Contradictions** between design and as built. **Incomplete** instrumentation records.
- 9 **Deficient** quality controls.
- 10 Short tunnels with stability problems at the portals. Insufficient lateral cover that led to inadequate confinement.

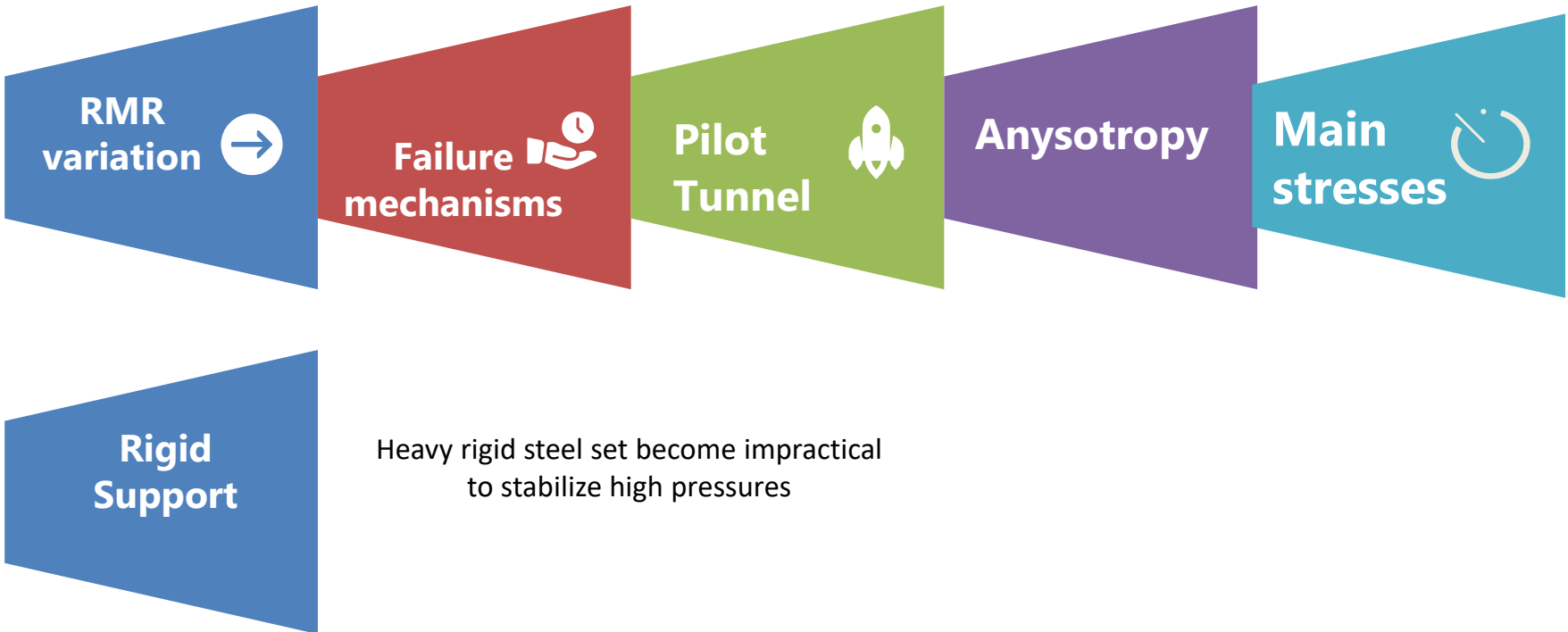
Support system design based purely on empirical methods related to a variation of the RMR geomechanical classification

Classification method did not cover failure mechanisms that usually occur in deep tunnels.

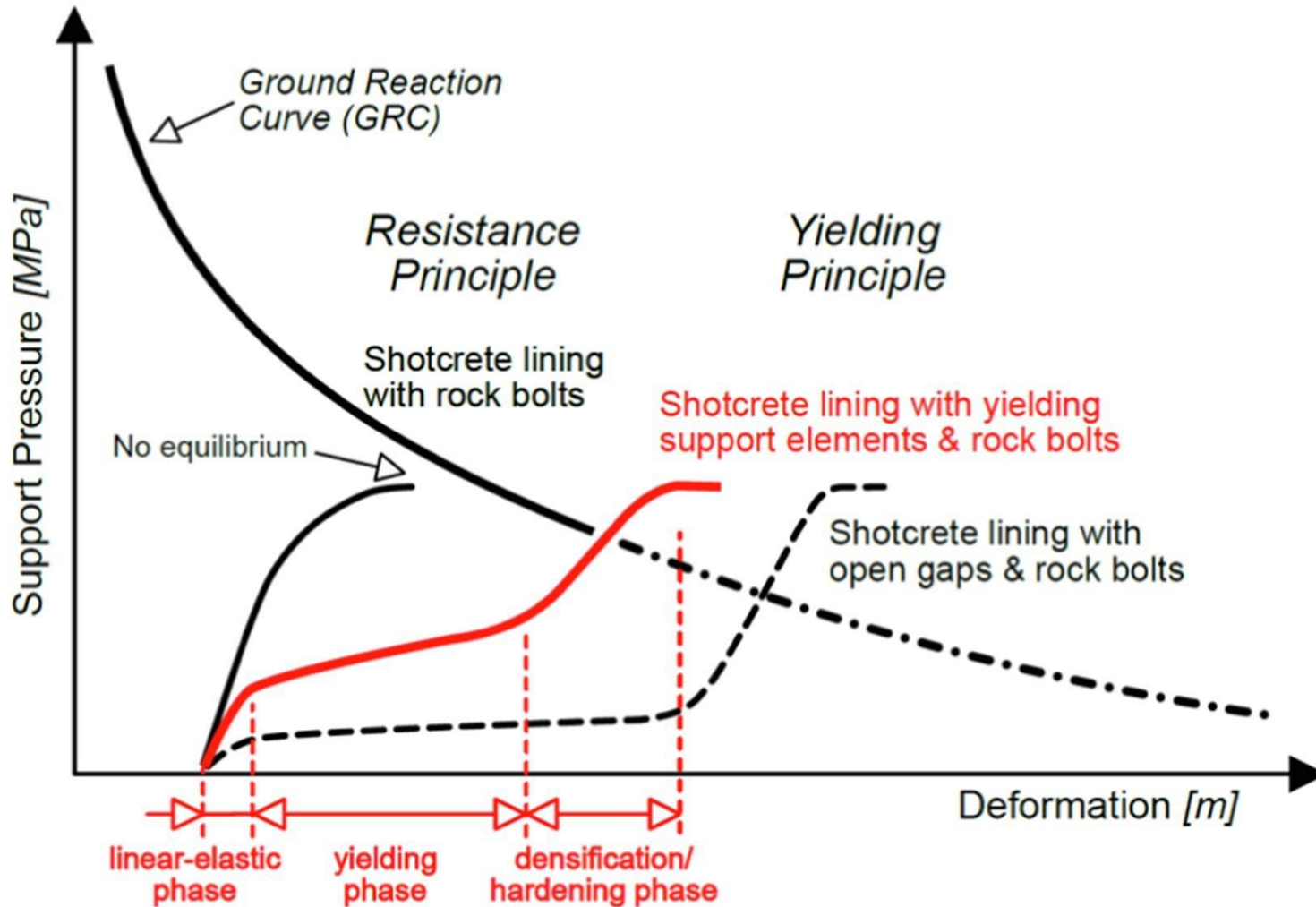
Findings from pilot tunnel, were not properly incorporated. Deformations >10-15% of the excavation diameter were encountered.

Anisotropic or time-dependent rock mass not considered. Nor relationship between the rock mass deformation and the support, nor the effect of the construction sequence

Geomechanical classification did not consider relationship between maximum and minimum in-situ stresses and the relationship with the type of rock, the geometry of the excavation

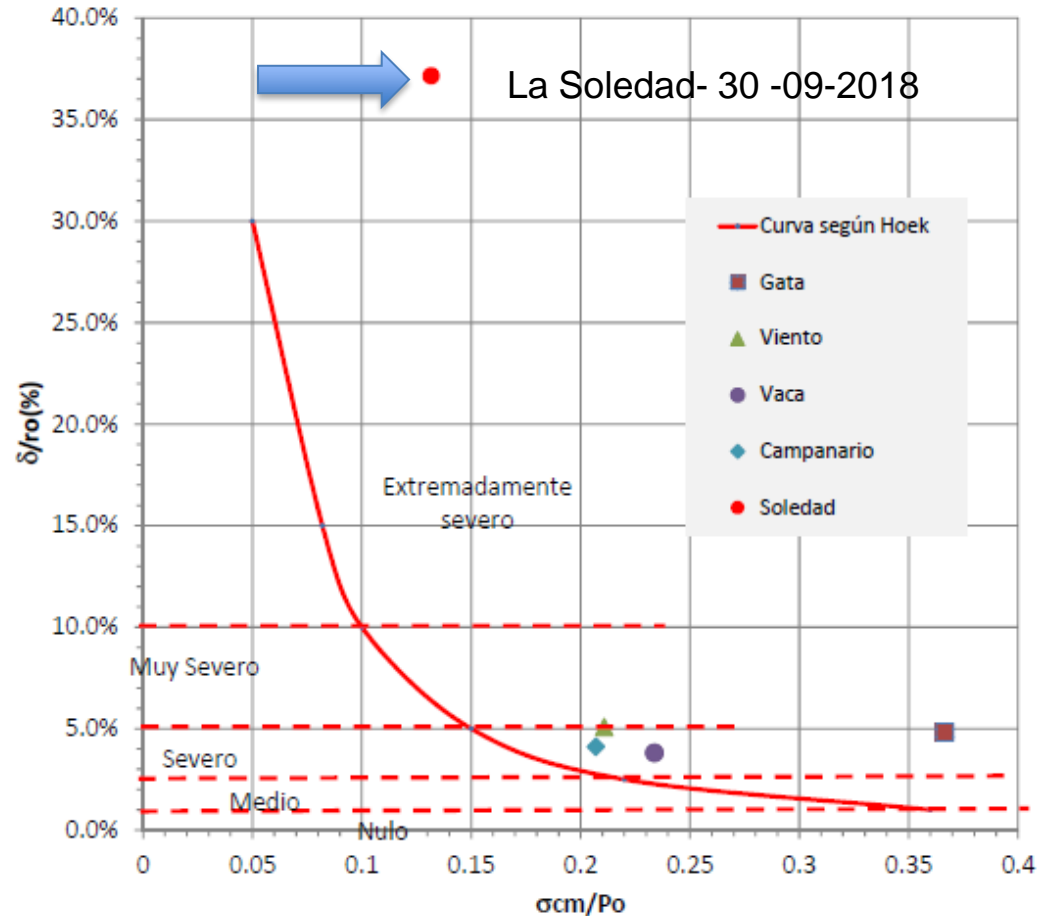


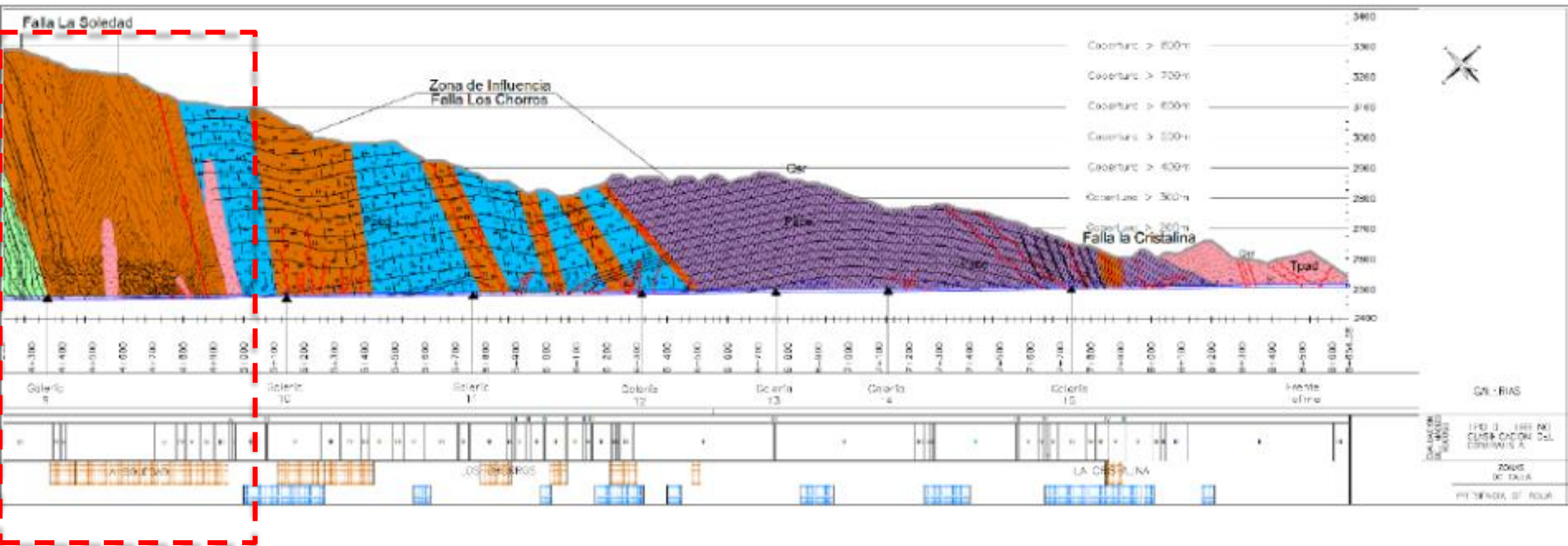
Heavy rigid steel set become impractical to stabilize high pressures



(Entfellner et al, 2023)

- Severe to extreme squeezing .
- Creep behaviour.
- Support with rigid Steel sets.
- Curved invert constructed late and incomplete.







Large displacements and damage to installed support



Damages to the steel sets and shotcrete

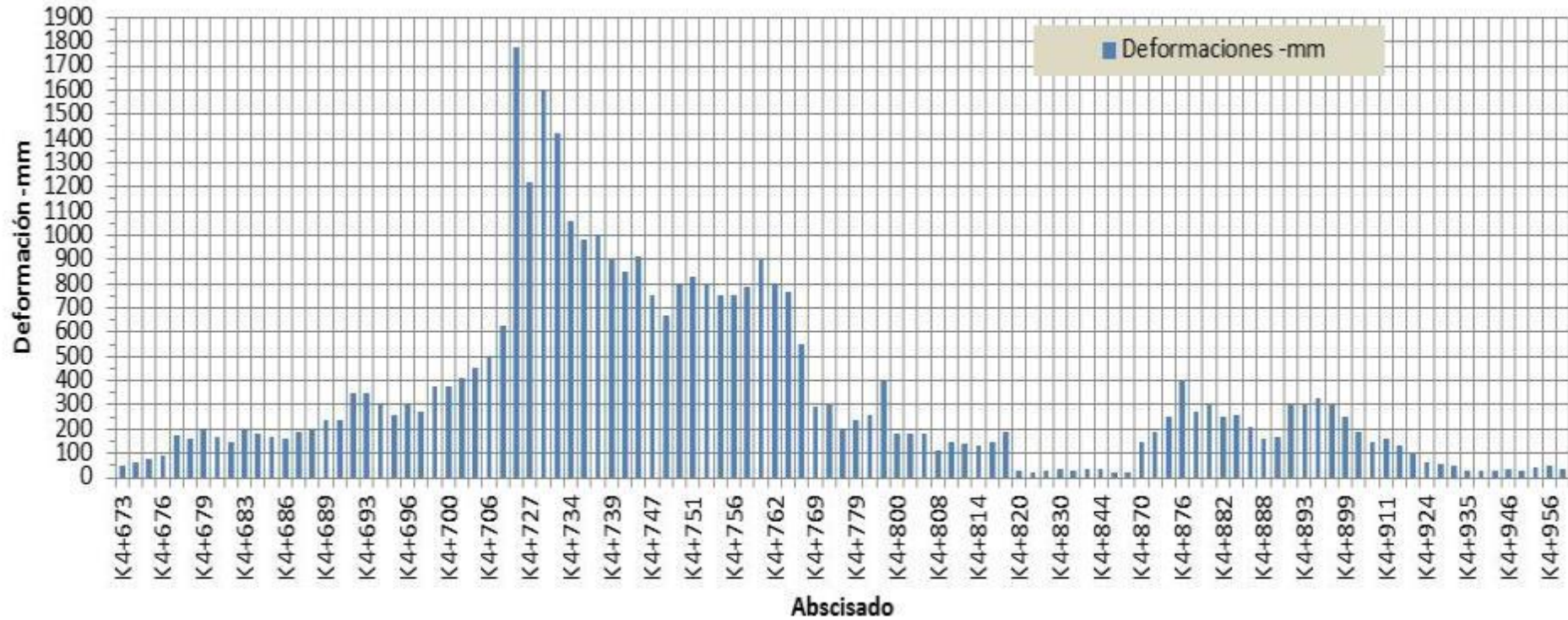


Measured convergence in the main tunnel

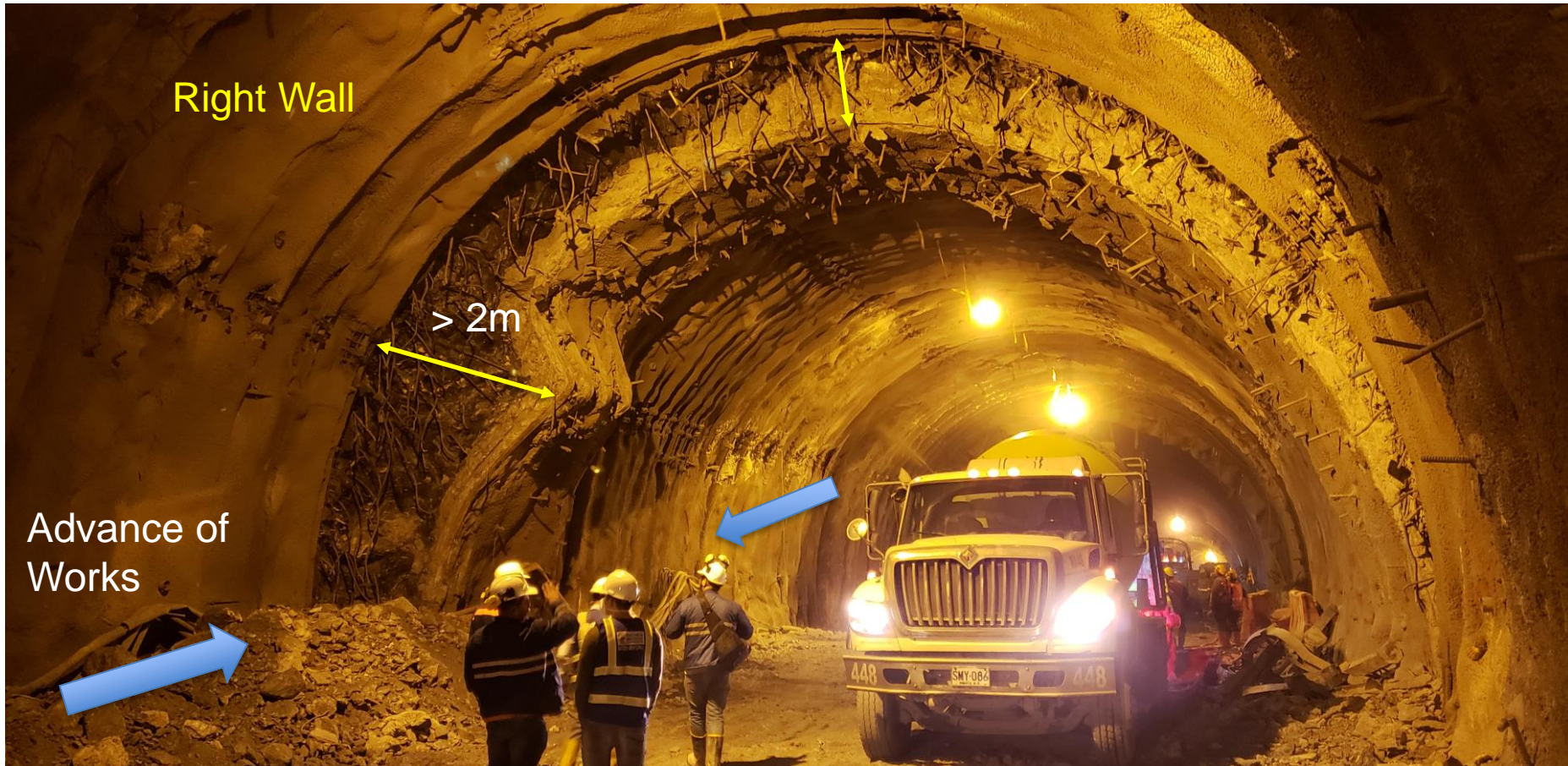


Deformed steel arches,
protrusion into the section
due to large displacements



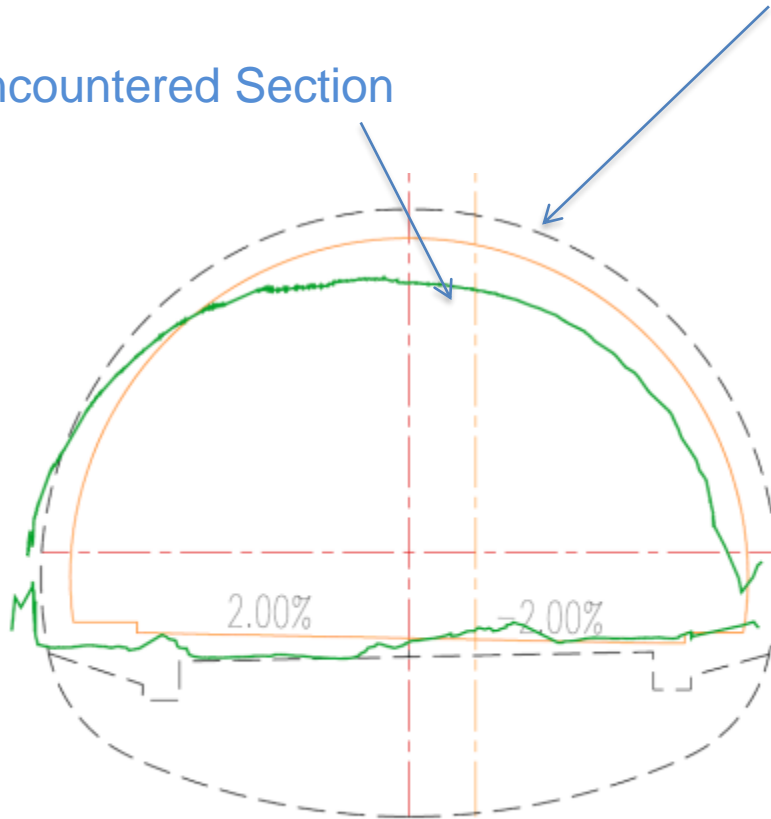


View towards Quindio



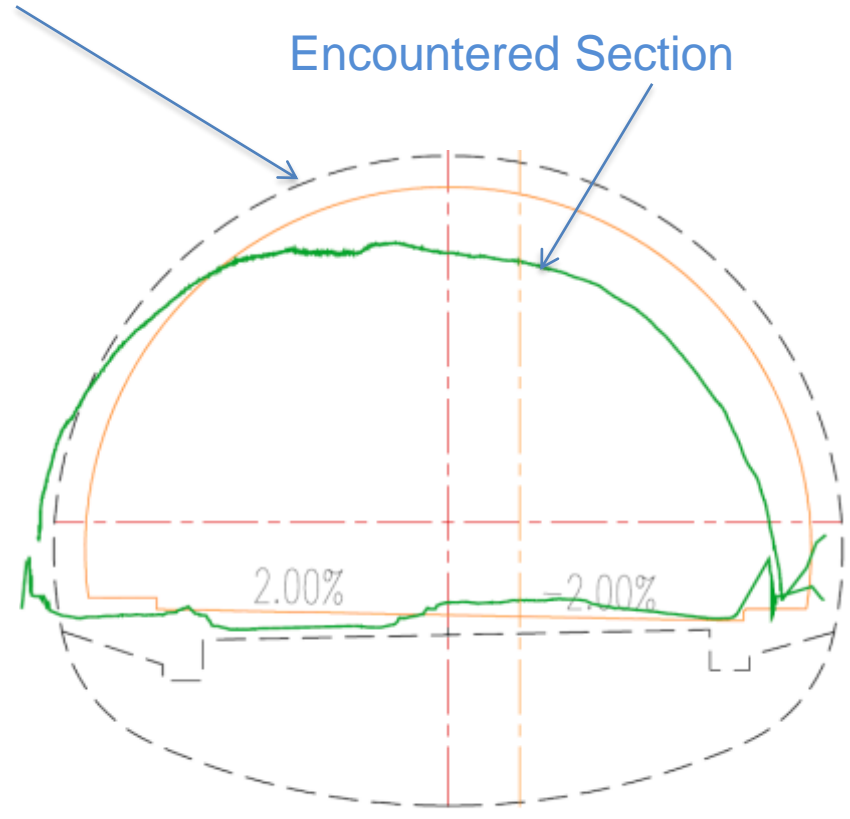
Theoretical Cross Section

Encountered Section



4+705.00
FALLA LA SOLEDAD

Encountered Section



4+710.00
FALLA LA SOLEDAD





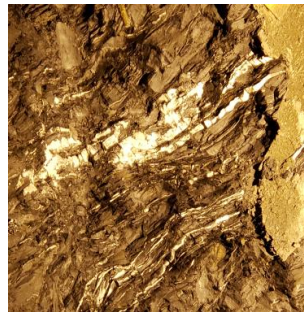


Pilot Tunnel



Rock mass Parameters

New tests,
Understand
anisotropy, back
calculate parameters



Detail of the rock mass in the La Soledad Fault Zone.

Analyze Instrumentation

Understand
effects of
construction
sequence

Creep

Acknowledge
creep and time
dependent
behavior

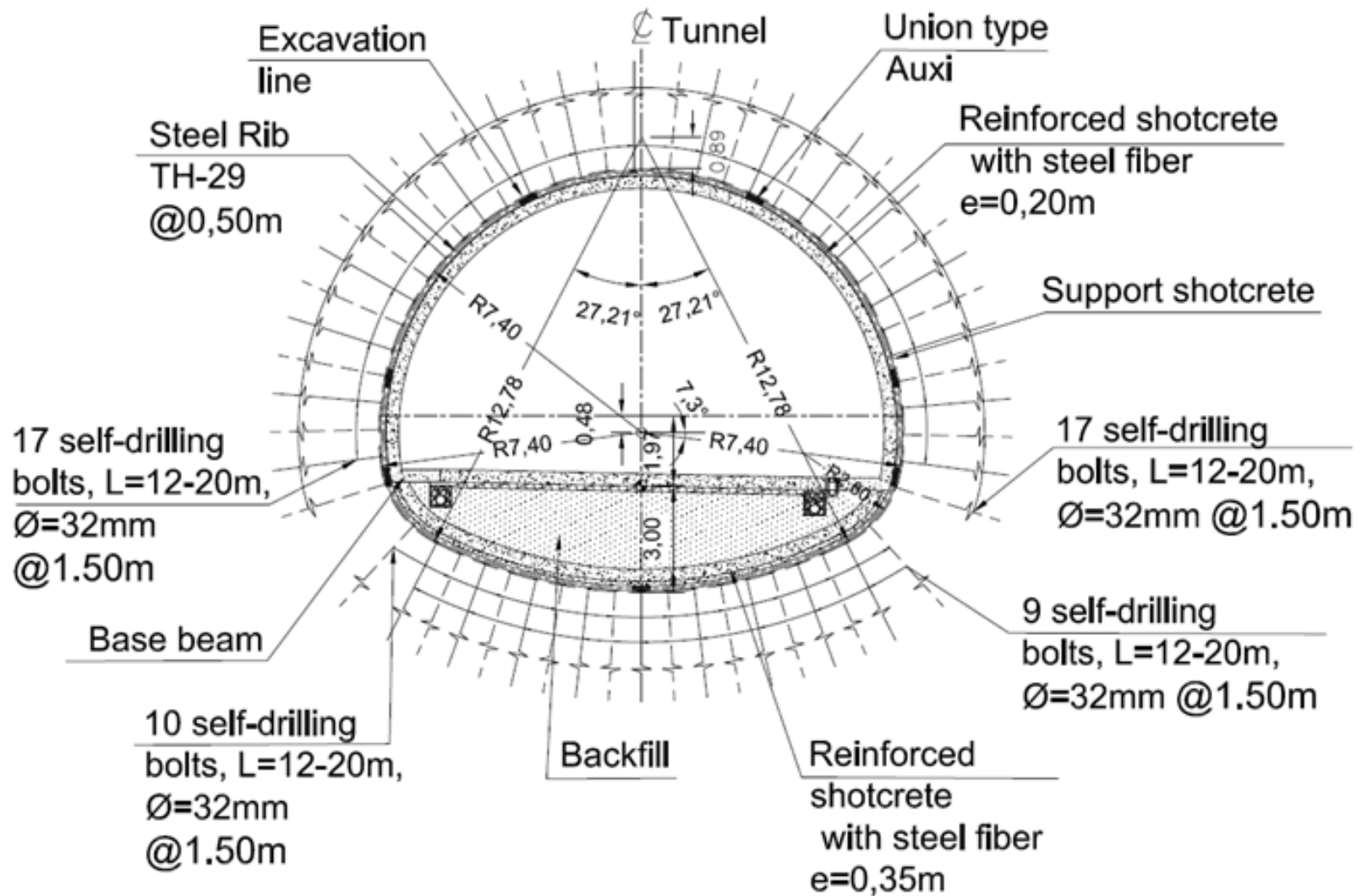
Flexible Supports

Yielding Supports
and closely
controlled
construction
sequence.

Observational Method

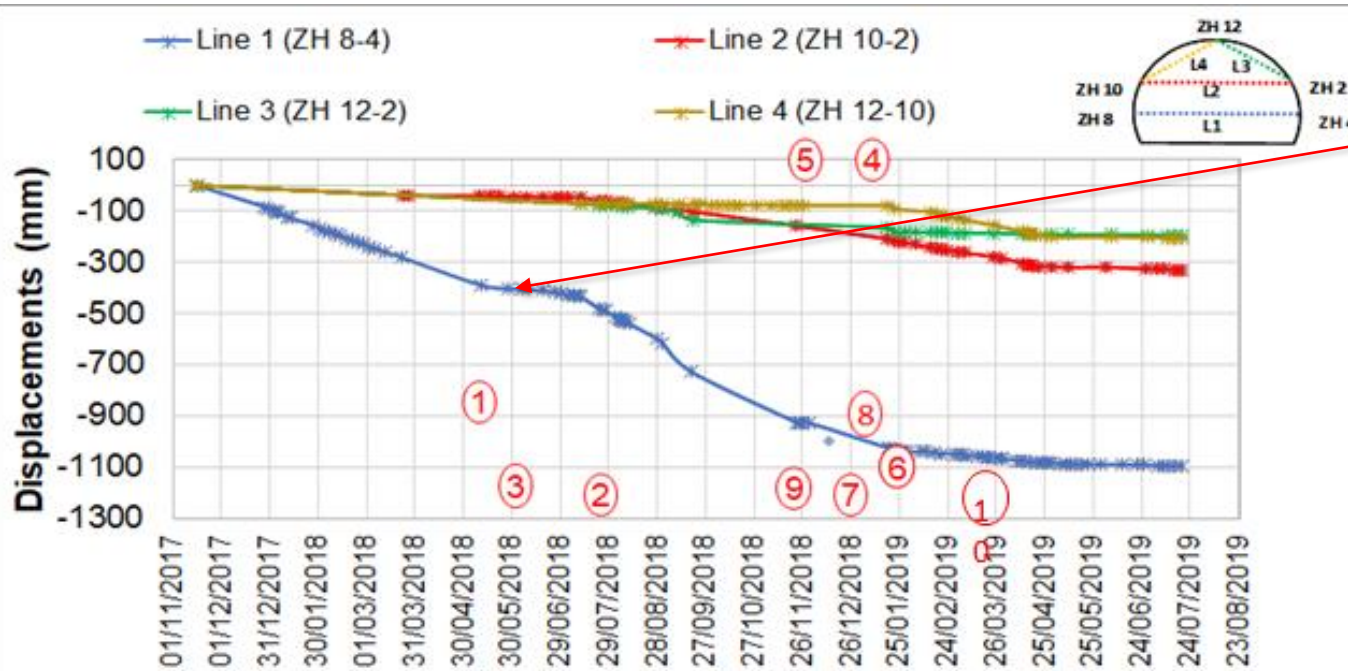
Extensive
instrumentation.
Analysis and adjustment
of support and
construction sequence.

Qualitative Evaluation	Maximum Displacement mm	Section Invasion cm	Damage to Support
Very High (A)	>300	>30	Bent and damaged steel sets, fissures in shotcrete, rockfalls
High (B)	150-300	15-30	Steel sets partially bent and/or fissures in shotcrete.
Medium(C)	50-150	5-15	Steel sets derailed and/or fissure in concrete
Low (D)	0-50	0-5	Small fissures in shotcrete
Null (E)	0	0	No damage

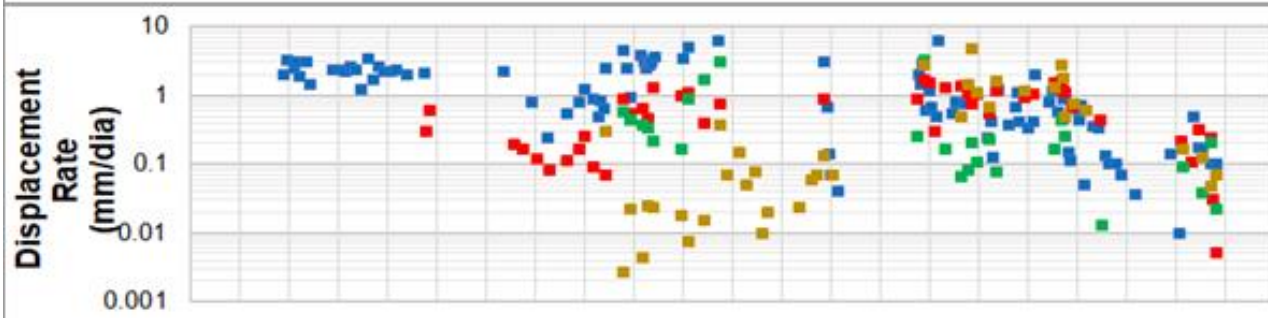




Treatment	Bolts	Reprofiling	Shotcrete (1 st layer)	Steel Sets	Shotcrete (2 nd Layer)	Shotcrete (3rd Layer)	Invert
A	L=12m @1.5x 1 (Selfdrilling)	Theoretical Line +0.1.5m	0.05+ fiber	Th-29 @ 1m	0.1+ fiber	0.05 @vault and walls+0.16 at invert+fiber	Curved with 2.15m
B	L=6m @1.5x 1 (Selfdrilling)	Theoretical Line	0.05+ fiber	Th-29 @ 1m	0.1+ fiber	0.05	Curved with 2m
C-1	NO	Theoretical Line	0.05+ fiber	HEB160 @1m	0.1+ fiber	0.05	Curved and straight
C-2	L=6m @1.5x 1 (Type A)	Theoretical Line	0.05+ fiber	HEB160 @1m	0.1+ fiber	0.05	Curved and straight
D	NO	Theoretical Line	0.05+ fiber	No	No	No	No



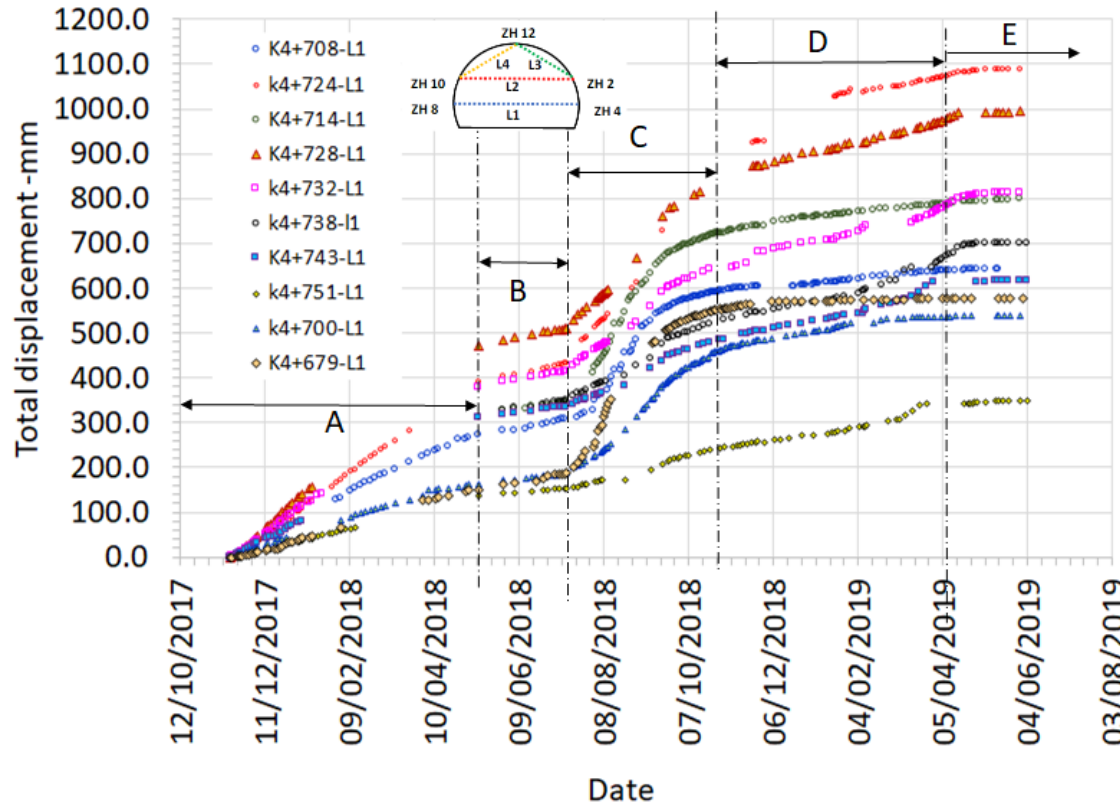
Activation of displacements upon removal of the base beam due to lack of support and joint action with curved invert.



1	Demolition of the base beam
2	Reprofiling
3	Bolts in vault and walls
4	Steel Rib
5	Curved invert excavation

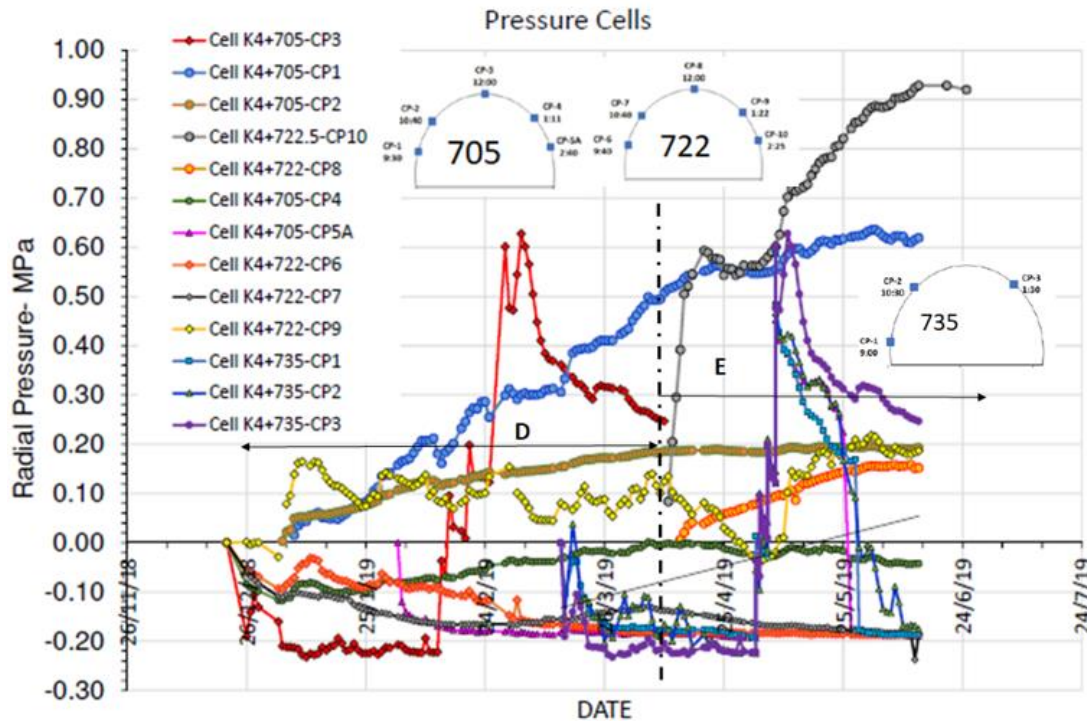
6	Steel rib in the invert- Right wall
7	Steel rib in the invert- Left wall
8	Bolt in the invert
9	Bolts - 20 m Long (Vault)
10	Closure of joints or windows

Convergence measured with tape extensometer



The behavior of the displacements allowed to distinguish five periods:

- (A) before intervening the tunnel with the rehabilitations works and since the beginning of the instrumentation measurements with tape extensometer in October 2017
- (B) when self-drilling rock bolts were installed.
- (C) when the base beam was removed and the reprofiling started.
- (D) during invert construction works
- (E) when yielding gaps were completely closed in May 2019.



- In the period prior to the windows closure (Period D) an increase in pressures was noted in several of the cells.
- After the gaps closure, there was a reduction in pressure rates and a general stabilization in most of the radial loads.
- In each of the stations there was an anisotropy of radial earth loads applied to the support.

- (A) before intervening the tunnel with the rehabilitations works and since the beginning of the instrumentation measurements with tape extensometer in October 2017
- (B) when self-drilling rock bolts were installed.
- (C) when the base beam was removed and the reprofiling started.
- (D) during invert works
- (E) when yielding gaps were completely closed in May 2019



Reprofiling @ the Soledad Fault-
K4+682 a K4+686



Reprofiling to install TH-29 Steel
sets. @K4+687





Installation of self drilling bolts

Installation of TH-29 Steel set-
K3+175- K3+176

Installation of self drilling bolts @
invert K4+670



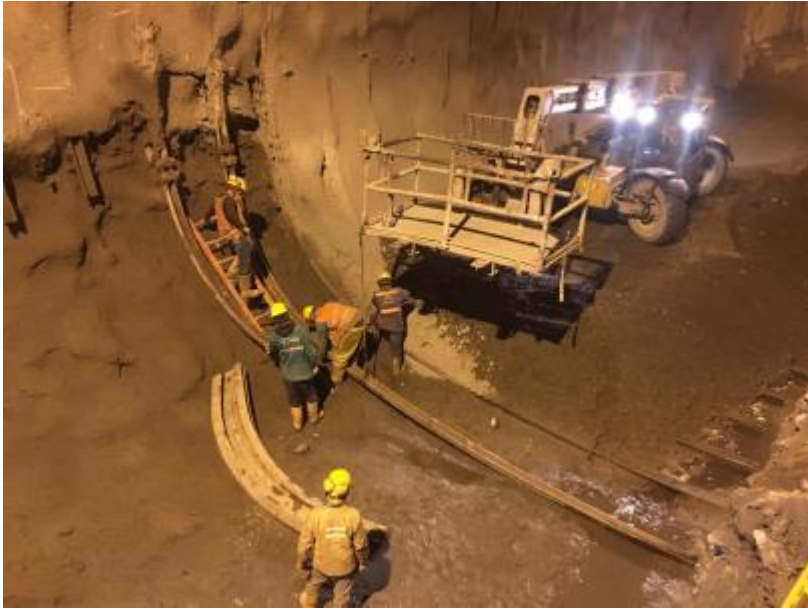
Reprofiling and demolition of base beam @ - K4+534



Installation of Steel sets @ curved invert.

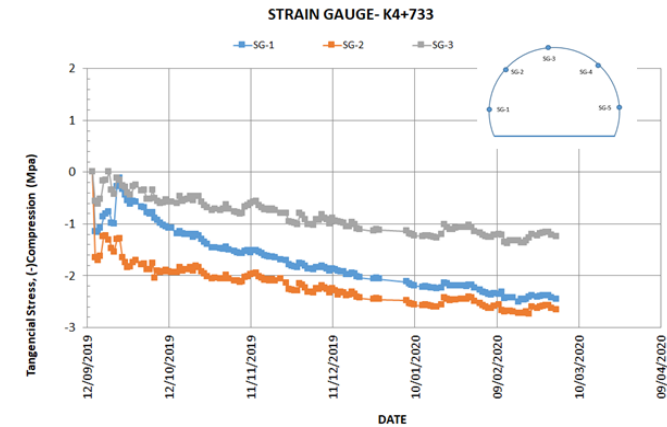
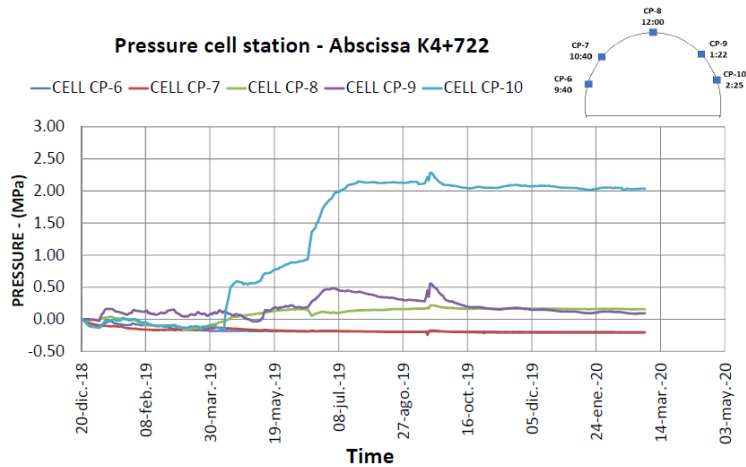
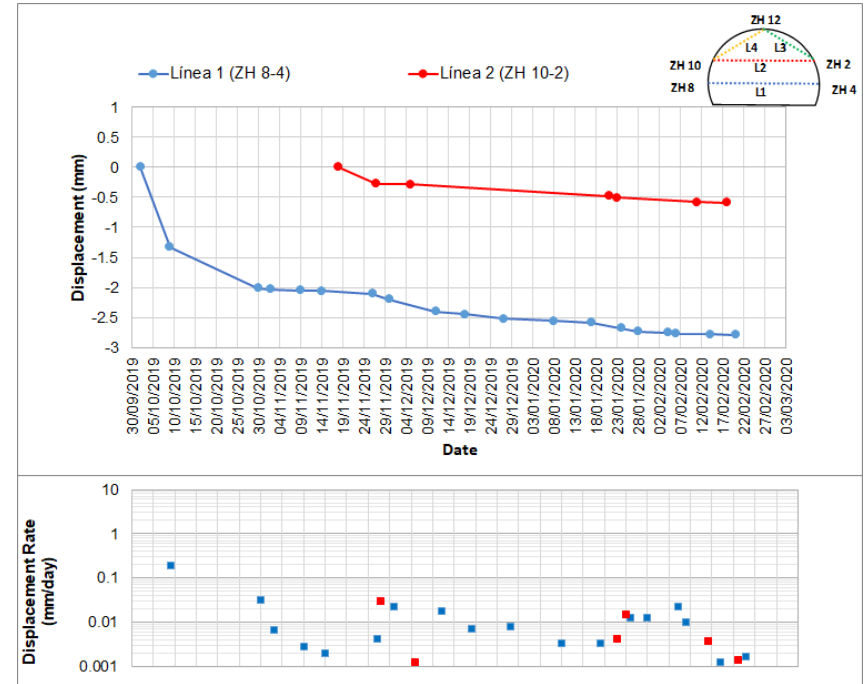


Initial Shotcrete and Steel sets for
invert @ K3+890 - K3+896



Shotcrete and invert Steel Sets
K4+683 a K4+685





Tangential stress deduced with vibrating wire strain gauges





The la Linea Tunnel is a relevant case study of the problems that arise from poor project structuring and contracting a tunnelling project as lump turnkey Project.



Underground Works demand special contractual provisions to be successful. Efficacy of design and construction methods are also linked to contractual provisions.



The Project Owner should own the ground related risk



The contractor should assume the performance related risk for a set of ground conditions defined in the GBR.



This the balanced and equitable risk distribution behind the ITA/FIDIC Emerald Book



Flexible non-rigid support are required to support the ground mass when squeezing ground is encountered.



Thorough geotechnical instrumentation properly and timely interpreted with the construction sequence can be fundamental for defining the required support even in extreme conditions and great uncertainty.

